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# Morphological evolution and grain size distribution of as-cast and solution treated Cu-Zn-Al alloy

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## Abstract

The development of ternary Cu-20Zn-6Al shape memory alloys was carried out using an oil-fired crucible furnace for casting. The experimental alloy's chemical, morphological, and grain size distributions were studied in both the as-cast and solution-treated states. The alloy's microstructure was observed and examined using optical metallurgical microscope; it revealed that solution treatment greatly refines and homogenizes the grains. Single martensite phase could be seen in optical micrographs of the as-cast ternary Cu-20Zn-6Al alloy. The martensitic phases required for the shape memory effect are present in both the as-cast and quenched alloys. The as-cast Cu-20Zn-6Al SMA has a grain size distribution of 10 to 110  $\mu$ m, whereas the solution-treated Cu-20Zn-6Al alloy has a grain size distribution of 60 to 150  $\mu$ m. Thermal processing and the holding interval before quenching was adduced to have encouraged the observed rapid grain development. Because of the anticipated improvement in mechanical and shape memory qualities as a result of the significant purification and homogeneity of grains observed after solution treatment, the produced alloys may be used in structural vibration damping applications

Keywords: Shape memory alloy, Grain size, Solution treatment, Cu-Zn-Al alloys, Martensitic transformation, microstructure.

## 1. Introduction

A type of intelligent/advanced materials known as shape memory alloys (SMAs) restore their shape after being subjected to thermal or deformation forces (Alaneme et al., 2022; Christofidou et al., 2017; Dasgupta, 2014; Dasgupta et al., 2014; Stošić et al., 2017). Their importance as engineering materials cannot be overstated. Their two primary phases are high temperature austenite and low temperature martensite, and they can switch between them by being heated to a specific temperature or being stressed (Guerioune et al., 2008). Due to SMAs' ability to remember their shape during the austenite phase, even after deformation, their original shape can be restored. This phenomenon, often referred to as shape memory effect or martensitic transformation, alters the solid's atomic structure and microstructure. The ability of SMAs to display a variety of characteristics, including thermoelasticity, superelasticity, and damping capacity, makes them special.

Despite the fact that many alloys exhibit shape memory behaviour, Cu-based SMAs have been of particular interest to researchers for shape memory, structural, and damping applications because they are the least expensive, have better electrical and thermal conductivities, and are easily processed and welded shape memory alloys with exploitable shape memory properties (Alkan et al., 2018; Dar et al., 2016; Saha et al., 2018; Sampath et al., 2019).

For the development of inexpensive thermal actuators and sensors, intelligent/smart pipe joints, and couplings for marine and petroleum engineering applications, copper-based SMAs are recommended. (Yin et al., 2021). Cu–Zn–Al alloy is the most investigated copper-based SMAs, because it has a larger percentage of strain recovery than other Cu-based SMAs (Alaneme & Umar, 2018). Additionally, they can be produced and fabricated in a variety of ways, although these alloys are brittle because of their coarse grain structure and have weak mechanical characteristics including low fracture toughness and fatigue strength (Alaneme & Okotete, 2016; Yan et al., 2017). Due to their coarse grain microstructure, strong elastic anisotropy, concentration of secondary phases, and presence of impurities at the grain boundaries, Cu-Zn-Al alloys have low mechanical strength (Alaneme et al., 2019; Tian et al., 2019).

A number of academics have studied many aspects in terms of how they affect the properties of SMAs, such as the micro-addition of new elements to the ternary SMAs, (Alaneme et al., 2019; Dasgupta, 2014), heat treatment and quenching methods (Dasgupta et al., 2014), thermomechanical treatment (Dar et al., 2016), surface improvement, modification, and various techniques for preparation. Several groundbreaking studies have shown that the quaternary addition of alloying elements as well as thermal treatments that purify grain boundaries, refine grains, and improve mechanical properties can improve some properties of Copper-based ternary SMAs such as superelasticity (ability to undergo large strains without plastic deformation or failure), shape memory effect, and the damping capacity (Lu et al., 2009). The goal of the current study is to design and develop a novel Cu-20Zn-6Al alloy and analyze how the solutionizing heat treatment affects the grain size and microstructure of the alloy.

### 2.0 Materials and Methods

The methodical approach used to carry out this study essentially entails alloy development via liquid metallurgy processing route using pure copper, zinc, and aluminum, solutionizing thermal treatment at 850°C and sample preparation from the as-cast and solutionized alloys for microstructural and grain size examinations.

## 2.1 Alloy Development

The Cu-Zn-Al alloys were developed by melting high purity copper, zinc, and aluminum (>99.97%) at a temperature of about 1200°C in an oil-fired crucible furnace. A mild steel 15mm diameter mold that had been preheated to 200–300°C was used for pouring and solidification of the molten alloy.

### 2.2 Solutionizing Heat Treatment

The as-cast alloys underwent a solution heat treatment at 850°C held for 10 minutes, followed by a direct quenching in water, to improve their chemical and microstructural homogeneity. These solutionizing parameters (temperature and time) were adopted because it was discovered that solution treating of Cu-Zn-Al SMAs for 10 minutes at 870°C produced a complete solution of the  $\alpha$ -phase with an appropriate grain size, (Asanovic et al., 2004). Solution treatment, also known as solutionizing involves heating the alloy above the solvus temperature and soaking it there until a homogenous solid solution is generated. The second stage is quenching, which involves rapidly cooling the solid to create a metastable, supersaturated solid solution  $\beta$ -phase that contains excess copper. Rapid quenching prevents  $\gamma$  precipitates from forming because the atoms do not have enough time to disperse to possible nucleation sites. This metastable  $\beta$ -phase must be retained in copper-based SMAs in order to get a good, reliable shape memory effect, which necessitates a sufficiently quick cooling from the betatizing temperature in order to prevent the  $\beta$ -phase from disintegrating into the equilibrium phases ( $\alpha$  and/or  $\gamma$ -phases) (Asanovic et al., 2000). Both the metastable  $\beta$ phase and martensite in these alloys undergo temperature-dependent diffusional transformations to a more stable structure at high temperatures, resulting in a corresponding loss of shape memory.

### 2.3 Alloy composition Analysis

Using an energy dispersive x-ray spectroscopy (EDS) technique, the as-cast and heat-treated Cu-Zn-Al shape memory alloy samples' elemental chemical compositions were examined, identified and quantified.

#### 2.4 Metallography and Grain Size Analysis

Using the optical microscopy (OM) technique, the microstructures of the generated alloys were characterized. Standard techniques were used to mechanically polish the specimens for optical rnetallography, and then they were etched in Nital etchant (ethyl alcohol + 2% HNO<sub>3</sub>) for optical inspection under metallurgical bench microscope (Model: L2004). The optical micrographs were subjected to image analysis using the imageJ program in order to determine the volume proportion of the intermetallic phases and grain characteristics of the microstructures. The samples were examined longitudinally and transversally. To enhance observation, the camera-captured optical image was then processed by adjusting the contrast, and a pseudo-color representation was used to aid with interpretation. The perimeter, area, and diameter of each grain were calculated once the image contrast was optimized. The summarized procedures for the alloy's structural and image analysis are surface preparation (cutting, grinding, polishing, and etching), microscopic examination and image acquisition, image processing, quantitative image analysis (size, shapes, and distribution of grains), and result interpretation (Alo et al., 2018; Edoziuno et al., 2020).

#### 3.0 Results and Discussion

#### 3.1 Chemical Composition

The bulk chemical composition of as-cast and solution-treated alloy samples were both determined (Table 1) using energy dispersive x-ray spectroscopy (EDS) analyses for metallic elements. To determine the variation in compositional measurements, the compositional analysis was performed twice. Taking into account the measurement error for the analysis technique of 1% of the absolute value, the measured elemental compositions reported for both as-cast and heat-treated samples were compatible with the specified composition of Cu-20-Zn-6Al. The significant burning and evaporation of zinc during the melting, pouring, and solutionizing procedures caused the observed decrease in zinc concentration (Dasgupta et al., 2014; Zhuo et al., 2020).

Table 1: Experimental chemical composition of the as-cast and solution-treated Cu-20Zn-6Al alloys.

Alloy	Cu (wt%)	Zn (wt%)	Al (wt%)
As-cast	72.92	19.18	5.55
Heat-treated	74.30	18.50	5.14

### 3.2 Metallographic Examinations

As shown in Figure 1a, the ternary Cu-20Zn-6Al alloy displays a sharp-edged, elongated grain structure of a single martensite phase. The martensite grain structures become more refined and dendritic with dendrite arms after solution treatment at 850°C (Figure 1b). As observed in the photomicrograph of the as-cast Cu-20Zn-6Al alloy, Cu-Zn-Al SMAs within the composition range taken into consideration in this work are frequently found to include sharp-edged directionally solidified grain features, (Alaneme & Umar, 2018). The black areas denote the fine  $\beta$ -phase (intermetallic compounds), and the light (bright) sections represent the  $\alpha$ -phase matrix network of the microstructures (Haleem et al., 2021). The Cu-20Zn-6Al alloy features  $\alpha$  (Fcc) +  $\alpha$  two-phase area in its composition. Prior to quenching, single  $\beta$ -phase grains are known to be a necessary condition for the presence of pseudo elastic behavior in Cu-based SMAs. (Dasgupta et al., 2014). To obtain the desired single-phase material,  $\alpha$ -phase must be removed from the microstructure (i.e., the microstructure should only include  $\beta$ -phase). The necessary ( $\alpha + \beta$ ) microstructure is achieved through quenching and homogenization in order to promote the evolution of a favorable texture during further processing. The structural characteristics described in earlier investigations and the microstructure results are in good accord. (Alaneme & Umar, 2018; Haleem et al., 2021). Both the as-cast and solution treated alloys have the ability to exhibit shape memory behavior, according to the obtained microstructure.



(a)

(b)

Figure 1: Optical micrographs of Cu-20Zn-6Al; (a) as-cast, and (b) solution-treated samples.

### 3.3 Grain Characteristics

The Cu-20Zn-6Al SMA's as-cast and solution-treated microstructural characteristics can be seen by image analysis utilizing the imageJ software. The grain size of the as-cast and solution-treated alloys varies significantly (Table 2). The table shows that the as-cast ternary alloy has smaller grains than the alloy that has been solution treated. Increased grain sizes are seen in the solution-treated sample, which was heated to 850°C before being quenched. Because the quenched sample had larger grains than the matching as-cast state, sudden quenching could not have stopped grain expansion. The development of grains has remained homogeneous in quenched samples as well. The martensitic phases required for shape memory behavior were expected to precipitate after quenching from high temperatures. The generated as-cast and solution-treated Cu-20Zn-6Al SMA's minimum, median, maximum, and average grain sizes are also shown in Table 2.

Sample	Std Dev.	Sum	Min	Median	Max	Count	<b>Total Area</b>	Average	%Area
								Size	
As-cast	22.52576	3297.025	10.53	65.184	108.595	3238	74003.854	22.855	11.403
Solution-	18.14876	5108.942	68.877	101.538	145.671	2441	230307	94.349	11.995
treated									

Table 2: Grain characteristics of as-cast and solution-treated Cu-20Zn-6Al alloy.

Figures 3a&b show the grain size distribution of the Cu-20Zn-6Al alloys both as-cast and solution-treated. A solid line representing the log-normal function of the statistical scale fits the grain diameter distribution in Figures 3a and 3b well (Nwaeju et al., 2021; Soltani et al., 2021). This suggests that the grains found in the microstructures were primarily made up of smaller grains, with a few bigger grains filling in the gaps. The grain size frequency distribution profile diagrams clearly show the most common grain sizes for both the as-cast and heat-treated alloys. The as-cast Cu-20Zn-6Al SMA has a grain size distribution of 10 to 110  $\mu$ m, whereas the solution-treated Cu-20Zn-6Al alloy has a grain size distribution of 60 to 150  $\mu$ m. The heat processing and holding duration before quenching are responsible for the observed fast grain growth. (Alaneme et al., 2021; Dasgupta, 2014; Pang et al., 2019). Previous research has shown that when heat treated at high temperatures, the grains of ternary Cu-based SMAs

without the inclusion of quaternary micro-additives grow quickly. (Agrawal & Kumar, 2018; Furlani et al., 2005; Xu, 2008; Xu et al., 2019).



Figure 3: Grain size distribution of Cu-20Zn-6Al alloys: (a) as-cast (b) Solution treated.

#### 4.0. Conclusion

The investigation's findings allow for the following deductions:

- i. A hitherto unresearched polycrystalline copper-based SMA was developed, and the microstructure and grain size properties in both the as-cast and heat-treated states were examined.
- ii. EDS elemental analysis showed the concentrations of the constituent elements in the as-cast and solutionized experimental alloys, with a decrease in the designed quantities of zinc due to quick evaporation of Zn at high temperature.
- iii. A single martensite phase could be seen in the optical micrographs of the ternary Cu-20Zn-6Al alloy, however after solution treatment at 850°C, the martensite grain structures become more distinct and dendritic, with dendrite arms. The martensitic phases required for shape memory behavior are present in both the as-cast and the quenched alloys.
- iv. The ternary Cu-20Zn-6Al alloy's grain size has grown noticeably quickly, according to the grain distribution, as a result of thermal treatment and holding time prior to quenching.

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